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[Thallium Free -] A Metal Halide Lamp with Magnesium Halide  
Filling For Improved Dimming Properties

TECHNICAL FIELD

5           This invention relates to high intensity discharge lamps  
and more particularly to high intensity discharge metal halide  
lamps. Still more particularly it relates to a metal halide  
filling for ceramic metal halide lamps. Ceramic metal halide  
lamps usually contain TlI and NaI in their filling. However,  
10       other known metal halide materials such as  $DyI_3$ ,  $HoI_3$ , and  $TmI_3$ ,  
are frequently used.

BACKGROUND OF THE INVENTION

15           This invention relates generally to high intensity dis-  
charge (HID) lamps and, more particularly, to metal halide  
lamps with ceramic discharge vessels having superior dimming  
characteristics. Low wattage metal halide lamps with their  
high efficacy have become widely used for interior lighting.  
Until now, almost all metal halide lamps were used for general  
20       lighting and have been operated at rated power. Due to the  
ever-increasing interest in energy conserving lighting sys-  
tems, some dimmable metal halide ballast systems are available  
on the market for metal halide lamps. Working under dimmed  
conditions (usually dimmed to as low as 50% of rated power),  
25       the performance of the regular metal halide lamps on the  
market deteriorate dramatically. Typically the color tempera-  
ture (CCT) increases significantly, while the color-rendering  
index (CRI) decreases. And the lamp hue will deteriorate from  
white to greenish or pinkish depending on the lamp's chemis-  
30       try. Furthermore the efficacy of the lamp usually decreases  
significantly.

          Under dimming conditions, the light emitted by commer-  
cially available metal halide lamps will have very strong  
green hue, which can be very objectionable for many indoor  
35       applications. The strong green hue in the light of dimmed

ceramic metal halide lamp is due to the radiation of Tl green lines (535.0 nm). Under dimming conditions, the discharge tube wall temperatures as well as its cold-spot temperature is much lower compared to the temperatures at rated power. At the lower cold-spot temperatures under dimming conditions, the ratio of partial pressure of TlI in the discharge tube is much higher compared to the partial pressures of other metal halides. Under dimming conditions, the relatively higher TlI partial pressure emits relatively stronger green Tl radiation at 535.0 nm. Since the Tl radiation at 535.0 nm is very close to the peak of the human eye sensitivity curve, higher lumen efficacy is achieved at rated power with TlI as one of the filling components in almost all commercial ceramic metal halide lamps.

With the present invention, superior lamp performance under dimming conditions with ceramic discharge vessel was achieved in nitrogen filled outer jackets at relatively high pressure between about 350 and 600 mmHg by a new chemical fill of the ceramic discharge tubes. In the newly invented lamps,  $MgI_2$  is used in the discharge tubes to replace the TlI in the fill composition of ceramic metal halide lamps.  $MgI_2$  is used to replace the TlI as one of the fill components because Mg has both green radiation for higher efficacy and has a similar vapor pressure variation with temperature as that of the rare earth iodides in the discharge tube dosing.

Due to the similar vapor pressure variation with temperatures,  $MgI_2$  partial pressure will drop under dimming conditions proportionally to that of the other rare-earth halides. This leads to a white lamp under dimming rather than the greenish hue of the lamps with TlI.

Also, the relatively higher vapor pressure of  $MgI_2$  at rated power results in relatively strong green radiation at 518 nm. Since the Mg radiation at 518.0 nm is very close to the peak of the human eye sensitivity curve, higher lumen efficacy is achieved at rated power with  $MgI_2$  as one of the

filling components. (Under some circumstances  $\text{MgBr}^2$  could be substituted for  $\text{TlI}$ ).

Therefore an objective of the present invention is to provide a [ceramic] metal halide lamp that when dimmed to about 50% power retains substantially its white hue.

Another objective of the present invention is to provide a [ceramic] metal halide lamp that when dimmed to about 50% power retains the CCT (correlated color temperature) substantially as in rated power.

Yet another objective of the present invention is to provide a [ceramic] metal halide discharge tube fill formulation that at rated power gives substantially similar performance (including efficacy, CRI, CCT and Duv) as the currently available products on the market.

Another objective of the present invention is to provide a [ceramic] metal halide lamp whose performance does not deteriorate under dimming, and whose outer jacket is filled with a gas at high pressure so that arcing is avoided at the end of life or if the outer jacket leaks during the lamp life.

Still another objective of the present invention is to provide a [ceramic] metal halide lamp that when dimmed to about 50% power its color-rendering index remains above 70.

#### DESCRIPTION OF RELATED PRIOR ART

Disadvantages of existing metal halide discharge lamps:

1. Existing metal halide lamps are optimized for a rated wattage without consideration of dimming performance.
2. When lamp power is reduced to about 50% of rated value the correlated color temperature increases dramatically often more than  $1000^\circ\text{K}$ . This change is not acceptable for most indoor applications.
3. When lamp power is reduced to about 50% of rated value the color rendering index decreases significantly.

4. When lamp power is reduced to about 50% of rated wattage the light radiated by the regular metal halide lamp has a color point, which is far away from the black body line, leading to a nonwhite hue.

5        There is no known publication on the filling materials of metal halide lamps with the purpose of improving dimming performance of metal halide lamps.

10        One patent application (application number 09/074,623 filed May 7, 1998 by Zhu et. al. by the same assignee) was filed on an invention of a new metal halide lamp which has significantly better lamp performance under dimming conditions. In that patent application, a lamp has a discharge tube burning in vacuum outer jacket to reduce convection heat loss from the cold-spot of the discharge tube, and a metal  
15        heat shield is used on the discharge tube to reduce radiation heat loss from the cold-spot during dimming. The invention shows very good dimming performance due to the fact that the thermal emissivity of the metal shield is much lower than that of a ceramic surface. Also the emissivity of the metal goes  
20        down as the temperature drops thereby keeping the cold-spot and vapor pressure of the salts substantially constant. A disadvantage of the invention is that widely used high voltage starting pulses on low wattage metal halide lamps in conjunction with a vacuum jacket may make the lamp susceptible  
25        to arcing when discharge tube leaks or slow outer jacket leaks exist.

30        U.S. Pat. No. 5,698,948 discloses a lamp that contains halides of Mg, Tl and one or several of the elements from the group formed by Sc, Y and Ln. The lamp filling also contains Mg to improve lumen maintenance. The lamp has a disadvantage of strong green hue when dimmed to lower than the rated power, due to the relatively higher vapor pressure of TlI under dimming conditions.

Lamps according to the present invention do not contain TlI in their chemical fill, so there is no hue change due to higher TlI vapor pressure under dimming conditions.

5 Lamps according to the present invention contain  $MgI_2$  as one of the main filling materials. The  $MgI_2$  is in a molar quantity between about 5 and 50% of the total molar quantity of the total halides. It replaces TlI for green light emission and to reach the same lumen efficacy as the commercial lamps containing Tl fills. The lamp, according U.S. Pat. No. 10 5,698,948, contains  $MgI_2$  as an addition to the filling ingredients just to improve lumen maintenance during lamp life. Through the addition of Mg to the lamp fill, according to the patent, one can influence the balance of one or several chemical reaction between Sc, Y and Ln with spinel ( $MgAl_2O_4$ ) to 15 such an extent that this balance is already achieved shortly after the beginning of lamp life, after which a further removal of the ingredients Sc, Y and Ln does not take place. Since the Mg addition is for reducing chemical reaction between the filling ingredients and the wall, the quantity of 20 Mg fill is based on the surface area of the inner wall of the discharge vessel.

Since  $MgI_2$  fill in the present invention is for light emission and for better lamp performance under dimming conditions, the optimization of the quantities of  $MgI_2$  fill are 25 based on the lamp performance under rated power as well as reduced power conditions, rather than the surface area of the discharge vessel.

#### DESCRIPTION OF DRAWINGS

30 FIG. 1 is an elevation view, partially in cross section, of a ceramic metal halide lamp.

FIG. 2 is an expanded cross-sectional view showing a configuration of a discharge tube in a first embodiment of the present invention.

FIG. 3 is a curve showing the color-rendering index (CRI) of a 100-hour photometry measurement of the lamps according to embodiment I and of a prior-art lamp, available on the market.

FIG. 4 is a curve showing the lamp efficacy in lumen per watt (LPW) of a 100-hour photometry measurement of the lamps according to embodiment I and of a prior art lamp, available on the market.

FIG. 5 gives the correlated color temperature (CCT) of a 100-hour photometry measurement of the lamps according to embodiment I and of a prior-art lamp, available on the market.

FIG. 6 gives the  $D_{uv}$  of a 100-hour photometry measurement of the lamps according to embodiment I and of a prior-art lamp, available on the market.

#### SUMMARY OF THE INVENTION

It is an object of the invention to provide a metal halide lamp in which a superior color performance is achieved under dimming conditions.

According to the invention, the ionizable filling of the lamp also comprises  $MgI_2$  in a molar quantity that lies between 10 and 50% of the total molar quantity of the total halides.

The lamp according to the invention has the advantage that the correlated color temperature of the lamps are hardly changed during a dimming operation, and the luminous efficacy of the lamp is not adversely affected by the new filling at rated power.

Elimination of TlI from the chemical filling has the advantage that the light radiated by the lamp has a color point which lies close to the black body line under both rated power and reduced power all the way to 50%.

The lamp of the present invention has significant advantages over lamps of the prior art during dimming performance. In the earlier patent application, (Zhu et. al., Application No. 09/074,633), a lamp must have an discharge tube burning in vacuum outer jacket to reduce convection heat

loss from the cold-spot of the discharge tube, and a metal heat shield is used on the discharge tube to reduce radiation heat loss from the cold-spot during dimming. Since high voltage starting pulses are general used on low wattage metal halide lamps to start the lamps. A lamp with vacuum jacket may make the lamp susceptible to arcing when the discharge tube leaks or a slow outer jacket leak exist. Also the use of the refractory metal heat shield may introduce higher lamp manufacturing cost.

With the lamp of the present invention, the ceramic metal halide lamps with superior dimming characteristics function in a nitrogen filled outer jacket which make the lamps much less susceptible to catastrophic failure during their life.

#### DESCRIPTION OF PREFERRED EMBODIMENTS

Referring to FIG. 1, the lamp 10 of the present invention includes a bulbous envelope 11 having a conventional base 12 fitted with a standard glass flare 16. Lead-in wires 14 and 15 extend from the base 12 through the flare 16 to the interior of the envelope 11, as is conventional. A harness formed of a bent wire construction 15, 15a is disposed within the envelope 11. The harness is anchored within the envelope on dimple 24. The harness 15, 15a and a conducting wire 14a support a discharge tube 20. The conducting wire 14a is welded onto the lead-in wire 14. A pair of straps 22a, 22b which are attached to harness 15a hold a shroud 23 which surrounds the discharge tube 20. A conventional getter 9 is attached to the harness 15a. Wires 30a, 30b supporting electrodes (not shown) are respectively attached to the harness 15a and the conducting wire 14a to provide power to the lamp and also provide support. Wires 30a, 30b are disposed within and hermetically sealed to a pair of narrow tubes 21a, 21b.

FIG. 2 is an expanded cross-sectional view showing a configuration of a discharge tube. In FIG.2, the discharge

5 tube 20 comprises the substantially cylindrical main tube 25,  
and first and second disks 28a and 28b disposed at openings of  
the both ends of the main tube 25, respectively. The main  
tube 25 and first and second disks 28a and 28b are made of the  
translucent ceramic material in which alumina is a main  
ingredient. The first and second disks 28a and 28b are  
integrated and fixed to the main tube 25 by a shrinkage  
fitting through a sintering process, so that the main tube 25  
is sealed airtight.

10 One end of the cylindrical narrow tube 21a is integrated  
with the first disk 28a by the shrinkage fitting. In a  
similar manner, one end of the cylindrical narrow tube 21b is  
integrated with the second disk 28b by the shrinkage fitting.  
A conductive sealing member 26a, a first lead-in wire 31a and  
15 first main electrode shaft 29a are integrated and inserted in  
the cylindrical narrow tube 21a. Specifically, one end of the  
first lead-in wire 31a is connected with one end of the  
sealing member 26a by a welding, and other end of the first  
lead-in wire 31a is connected with one end of the first main  
20 electrode shaft 29a by the welding. Then, the sealing member  
26a is fixed to the inner surface of the cylindrical narrow  
tube 21a by a frit 27a in a manner that the cylindrical narrow  
tube 21a is sealed airtight. When the sealing member 26a, the  
first lead-in wire 31a and first main electrode shaft 29a are  
25 disposed in the cylindrical narrow tube 21a, the other end  
part of the sealing member 26a is led outside the cylindrical  
narrow tube 21a, and serves as the outer lead-in wire 30a.

Furthermore, an electrode coil 32a is integrated and  
mounted to the tip portion of the other end of the first main  
30 electrode shaft 29a by the welding, so the first main  
electrode 33a is configured by the first main electrode shaft  
29a and the electrode coil 32a. The first lead-in wire 31a  
serves as a lead-in part of disposing the first main electrode  
33a at a predetermined position in the main tube 25. The  
35 sealing member 26a is formed by a metal wire of niobium. For



example, diameter of the sealing member 26a is 0.9 mm, and diameter of the first main electrode shaft 29a is 0.5 mm.

Similarly, in FIG. 2, a conductive sealing member 26b, a first lead-in wire 31b and first main electrode shaft 29b are integrated and inserted in the cylindrical narrow tube 21b. Specifically, one end of the first lead-in wire 31b is connected with one end of the sealing member 26b by a welding, and other end of the first lead-in wire 31b is connected with one end of the first main electrode shaft 29b by the welding. Then, the sealing member 26b is fixed to the inner surface of the cylindrical narrow tube 21b by a frit 27b in a manner that the cylindrical narrow tube 21b is sealed airtight. When the sealing member 26b, the first lead-in wire 31b and first main electrode shaft 29b are disposed in the cylindrical narrow tube 21b, the other end part of the sealing member 26b is led outside the cylindrical narrow tube 21b, and serves as the outer lead-in wire 30b.

Furthermore, an electrode coil 32b is integrated and mounted to the tip portion of the other end of the first main electrode shaft 29b by the welding, so the first main electrode 33b is configured by the first main electrode shaft 29b and the electrode coil 32b. The first lead-in wire 31b serves as a lead-in part of disposing the first main electrode 33b at a predetermined position in the main tube 25. The sealing member 26b is formed by a metal wire of niobium. For example, the diameter of the sealing member 26b is 0.9 mm, and the diameter of the first main electrode shaft 29b is 0.5 mm.

In a practical realization of a lamp according to the invention, the discharge vessel is made of polycrystalline alumina. The main electrode shafts and electrode coils are made of tungsten. The lead-in wires of the electrodes are molybdenum. The conductive sealing members of the electrodes are niobium. The rated power of the lamp is 150W. The filling of the discharge vessel was 10.5 mg Hg and 7.6 mg of the metal halides NaI, HoI<sub>3</sub>, TmI<sub>3</sub> and MgI<sub>2</sub> in a molar ratio

42:6:29:23. The total molar quantity of halides of Na, Dy, Ho and Tm is between about 50 and 95%. In addition, the filling comprises Ar or Xe with a filling pressure of 160 mbar as an ignition gas.

5           FIGS. 3 to 6 show the comparison results of lamps with present invention and a commercial ceramic metal halide lamp. The lamps were operated with a reference ballast and measured in a two meter integrating sphere under IES reference conditions. The data was acquired with a CCD-based computerized data acquisition system. All data presented in FIGS. 3  
10 to 6 were obtained with the operating position of the lamp being vertical base up. The experiments, for which the data is presented in FIGS. 3 to 6, were conducted using 150W ceramic metal halide discharge tube.

15           During operation of the lamps according to the present invention, and when comparing them to standard lamps, we found the standard lamps turned greenish on dimming and deviated substantially from the black body locus upon dimming to about 50%. When lamps with chemical fills from this invention were  
20 dimmed to about 50%, they still remained substantially on the black body locus, had no greenish hue, and generally looked white. Such color was satisfactory to the eye and it was substantially impossible to discern any color or hue change under dimmed conditions.

25           FIG.3 shows the changes of color rendering index (CRI) when lamps are dimmed. It can be seen that the CRI of the lamp according to the invention changed less than the standard lamp when the lamp was dimmed to 50% of its rated power.

30           FIG.4 shows the changes of lamp efficacy-lumen per watt (LPW) when lamps are dimmed. It can be seen that the LPW of the lamp according to the invention and the standard lamp changes in a very similar fashion when dimmed to 50% power.

35           FIG. 5 shows the changes of correlated color temperature (CCT) when lamps are dimmed. It can be seen that the CCT of the lamp according to the invention did not have significant

change when the lamp was dimmed to 50% of its rated power. With the prior art lamp, the CCT change was significant when the lamp was dimmed to 50% of its rated power.

FIG.6 shows the changes of lamp  $D_{uv}$  when lamps are dimmed. As is well known  $D_{uv}$  is a measure of the deviation from the black body. It can be seen that the  $D_{uv}$  of the lamp according to the invention did not have significant change when the lamp was dimmed to 50% of its rated power. With the prior art lamp, the  $D_{uv}$  change was significant when the lamp was dimmed to 50% of its rated power.

Therefore one can conclude that the lamps according to our formulation, containing  $MgI_2$  instead of  $TlI$ , perform comparably to the standard lamps at rated power. This performance includes efficacy, CCT, CRI and  $D_{uv}$  (which is a measure of how close the light source is to the black body curve). Furthermore, when standard lamps are dimmed to 50% power level their performance deteriorates substantially. What is most disturbing, in this deterioration, from the end user's point of view is the change in CCT and hue which is given by  $D_{uv}$ . As shown above these problems are eliminated by the substitution of  $TlI$  by  $MgI_2$  in the present invention. The lamps of the present invention remain at the same CCT and are unchanged in terms of hue remaining white throughout the dimming range.

It is apparent that modifications and changes may be made within the spirit and scope of the present invention, but it is our intention only to be limited by the following claims.

As our invention we claim: